A gas turbine is connected to a compressor and a generator through shafts and couplings with stiffness and moment of inertia as shown on the diagram.


$$
\begin{gathered}
\text { Compressor } \quad \begin{array}{c}
\text { Coupling } \quad \text { Turbine } \quad \text { Coupling } \quad \text { Generator } \\
I=10 \mathrm{~kg} \mathrm{~m}^{2} \quad \mathrm{I}=1 \mathrm{~kg} \mathrm{~m}^{2} \mathrm{I}=5 \mathrm{~kg} \mathrm{~m}^{2} \mathrm{I}=1 \mathrm{~kg} \mathrm{~m}^{2} \mathrm{I}=5 \mathrm{~kg} \mathrm{~m}^{2} \\
\mathrm{k}_{\mathrm{t}_{1}}=\mathrm{k}_{\mathrm{t}_{2}}=2 \mathrm{MNN} \mathrm{~m} / \mathrm{rad} \quad \mathrm{k}_{\mathrm{t}_{3}}=\mathrm{k}_{\mathrm{t}_{4}}=1 \mathrm{MN} \mathrm{~m} / \mathrm{rad}
\end{array}
\end{gathered}
$$

Severe torsional observations occur when running at the normal speed of $50 \mathrm{rev} / \mathrm{s}$. Neglect the inertia of the shafts and determine the fundamental natural frequency and the mode shape. Use Holzer's method to do this.

## SOLUTION

There are five moments of inertia and four shaft sections. From left to right these are
$\mathrm{I}_{1}=10 \quad \mathrm{I}_{2}=1 \mathrm{I}_{3}=5 \mathrm{I}_{4}=1 \mathrm{I}_{5}=5 \mathrm{k}_{\mathrm{t} 1}=\mathrm{k}_{\mathrm{t} 2}=2 \times 10^{6} \quad \mathrm{k}_{\mathrm{t} 3}=\mathrm{k}_{\mathrm{t} 4}=1 \times 10^{6}$
The equations to be solved using Holzers method are
$\mathrm{y}_{1}=1$
$\mathrm{y} 2:=\mathrm{y} 1-\frac{\omega^{2} \cdot \mathrm{I} 1 \cdot \mathrm{y} 1}{\mathrm{k} 1}$
$\mathrm{y} 3:=\mathrm{y} 2-\frac{\omega^{2}}{\mathrm{k} 2} \cdot(\mathrm{I} 1 \cdot \mathrm{y} 1+\mathrm{I} 2 \cdot \mathrm{y} 2)$
$\mathrm{y} 4:=\mathrm{y} 3-\frac{\omega^{2}}{\mathrm{k} 3} \cdot(\mathrm{I} 1 \cdot \mathrm{y} 1+(\mathrm{I} 2 \cdot \mathrm{y} 2+\mathrm{I} 3 \cdot \mathrm{y} 3))$
$\mathrm{y} 5:=\mathrm{y} 4-\frac{\omega^{2}}{\mathrm{k} 4} \cdot(\mathrm{II} 1 \cdot \mathrm{y} 1+(\mathrm{I} 2 \cdot \mathrm{y} 2+\mathrm{I} 3 \cdot \mathrm{y} 3)+\mathrm{I} 4 \cdot \mathrm{y} 4)$
$\mathrm{T} 1:=\omega^{2} \cdot \mathrm{I} 1 \cdot \mathrm{y} 1$
$\mathrm{T} 2:=\mathrm{T} 1+\omega^{2} \cdot \mathrm{I} 2 \cdot \mathrm{y} 2$
$\mathrm{T} 3:=\mathrm{T} 2+\omega^{2} \cdot \mathrm{I} 3 \cdot \mathrm{y} 3$
$\mathrm{T} 4:=\mathrm{T} 3+\omega^{2} \cdot \mathrm{I} 4 \cdot \mathrm{y} 4$
$\mathrm{T} 5:=\mathrm{T} 4+\omega^{2} \cdot \mathrm{I} 4 \cdot \mathrm{y} 4$
These must evaluated for various values of $\omega$ and the value when $\mathrm{T}_{5}=0$ found.

There should be a clue that this might be around $50 \mathrm{rev} / \mathrm{s}$ or $50 \times 2 \times \pi=314 \mathrm{rad} / \mathrm{s}$ or some multiple. However solving on a computer shows the following.


Finding the correct values by method would probably take all day with a calculator so one wonders what the examiner had in mind.

Evaluating in steps of $100 \mathrm{rad} / \mathrm{s}$ might have been advised.

| $\omega$ | 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{~T}_{5} \times 10^{-6}$ | 0 | 0.16 | 0.55 | 0.82 | 0.57 | -0.43 | -2.08 | -3.56 | -3.2 | 1.73 |
| $\mathrm{Y}_{2}$ | 1.0 | 0.95 | 0.8 | 0.55 | 0.2 | -0.25 | -0.8 | -1.45 | -2.2 | -3.05 |
| $\mathrm{Y}_{3}$ | 1.0 | 0.89 | 0.58 | 0.07 | -0.62 | -1.47 | -2.46 | -3.54 | -4.7 | -5.86 |
| $\mathrm{Y}_{4}$ | 1.0 | 0.74 | 0.035 | -0.90 | -1.75 | -2.07 | -1.35 | 0.95 | 5.34 | 12.26 |
| $\mathrm{Y}_{5}$ | 1.0 | 0.56 | -0.52 | -1.81 | -2.61 | -2.15 | 0.25 | 4.98 | 11.95 | 20.45 |

There is a critical frequency between 400 and $500 \mathrm{rad} / \mathrm{s}$ and between 800 and $900 \mathrm{rad} / \mathrm{s}$. These could be narrowed down further but in an exam it might be reasonable to guess at $450 \mathrm{rad} / \mathrm{s}$ and $950 \mathrm{rad} / \mathrm{s}$. Note that the higher one is around three times the running speed so his might account for the vibration.

To find the node, we need the deflections at the critical speed. Guestimate the values and plot.

| $\omega$ | 450 | 850 |
| :--- | :--- | :--- |
| $\mathrm{Y}_{1}$ | 1 | 1 |
| $\mathrm{Y}_{2}$ | 0 | -2.7 |
| $\mathrm{Y}_{3}$ | -1 | -5 |
| $\mathrm{Y}_{4}$ | -1.9 | 9 |
| $\mathrm{Y}_{5}$ | -2.4 | 16 |



At the lower speed there is a node close to the first coupling. At the higher speed there are two nodes, one in the first section and one in the third section of shaft.

